

PYCALC-LES

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# SCHEDULE, DAY 1

- Lecture
  - Presentation of **pyCALC-LES**
- Workshop
  - Working with **pyCALC-LES**
- Lecture
  - LES & DES **eBook**
- Workshop
  - Working with **pyCALC-LES**

# SCHEDULE, DAY 2

- Lecture
  - PANS & synthetic inlet b.c. [eBook](#)
- Workshop
  - Working with **pyCALC-LES**
  - Individual break-out Zoom meetings
- Lecture
  - Machine Learning: Neural network and EARSM
  - `slides-EARSM-slides-flow-induced-acoustic-seminar-huadong.pdf`
  - Paper can be downloaded [here](#)
- Workshop
  - Assignment on NN for improving a  $k - \varepsilon$  model can be found [here](#)
  - Python scripts for EARSM can be downloaded [here](#)
  - Assignment on NN for improving EARSM in recirculating flow can be found [here](#)
  - Working with Neural Network
  - Individual break-out Zoom meetings
  - Working with **pyCALC-LES** , **pyCALC-RANS** or [rans-k-eps-NN.py](#)

# SCHEDULE, DAY 3

- Lecture

- PINN (Physics-Informed Neural Network)
- `slides-machine-learning-k-omega-PINN-pinn.pdf`
- Paper can be downloaded [here](#)

- Workshop

- Working with PINN and **pyCALC-RANS**
- Python scrips can be downloaded [here](#)
- Individual break-out Zoom meetings

- Lecture

- Machine Learning: improving wall functions. Download [slides](#)

- Workshop

- Working with KDTree. Folder:  
`channel-16000-IDDES-wall-functions-nj98-kdtree-mean-from-backflow-A`
- Section 29 in [eBook](#)
- Individual break-out Zoom meetings

# FLOW CHART

## pyCALC-LES flowchart [▶ Link](#)

There are four main case-specific routines in each subdirectory

- `generate*.py` (`generate-channel-grid.py`, `generate-bound-layer-grid.py`, ...)
- `setup_case.py`
- `modify_case.py`
- `pl*.py` (`pl_uvw.py`, `plot_inlet.py`, ...)

The main program

- `pyCALC-LES-GPY.py`
- `synt_fluct.py`

- Generate simple Cartesian meshes

SECTION 0 choice of CPU or GPU

SECTION 1 choice of differencing scheme

SECTION 2 turbulence models

SECTION 3 restart/save

SECTION 4 fluid properties

SECTION 5 relaxation factors

SECTION 6 number of iteration and convergence criteria

SECTION 7 all variables are printed during the iteration at node

SECTION 8 time-averaging

SECTION 9 residual scaling parameters

SECTION 10 boundary conditions

## MODIFY\_CASE.PY

```
def modify_init(u3d,v3d,w3d,k3d,om3d,eps3d,vis3d,dist3d):  
def modify_inlet():  
def modify_conv(convw,convs,convl):  
def modify_u(su3d,sp3d):  
def modify_v(su3d,sp3d):  
def modify_w(su3d,sp3d):  
def modify_k(su3d,sp3d,gen):  
def modify_eps(su3d,sp3d):  
def modify_om(su3d,sp3d,comm_term):  
def modify_outlet(convw):  
def modify_fk(fk3d):  
def modify_vis(vis3d):  
def def fix_k():  
def def fix_omega():  
def def fix_eps():
```



# CREATE EXECUTABLE

The bash script `run-python` is used which reads

```
#!/bin/bash # delete first line
sed '/setup-case()/d' setup-case.py > temp_file
# add new first line plus global declarations
cat ../global-GPU temp_file modify-case.py ../STG-GPU.py
../synt-fluct-GPU.py ../pyCALC-LES-GPU.py > temp_file1;
# find setting of 'gpu'
'grep' gpu setup-case.py > gpu_value;
# remove leading white space
sed -i 's/^[ ] * //' gpu_value;
# add value of 'gpu' at first line
cat gpu_value temp_file1 > exec-pyCALC-LES-GPU.py;
/anaconda3/bin/python -u exec-pyCALC-LES-GPU.py > out
```

# GLOBAL DECLARATIONS

They are made in the file `global-GPU` which reads

```
global acrank,acrank_conv, acrank_conv_keps, acrank_conv_kom,  
... w_bc_south, w_bc_south_type, w_bc_west, w_bc_west_type,  
w_bc_z, w_bc_z_type, wale, x2d, xp2d, y2d, yp2d, zmax
```

# FULLY-DEVELOPED CHANNEL FLOW, $Re_\tau = 500$ , DNS

- `generate-channel-grid.py`
- `setup_case.py`
- `modify_case.py`

# THE GRID

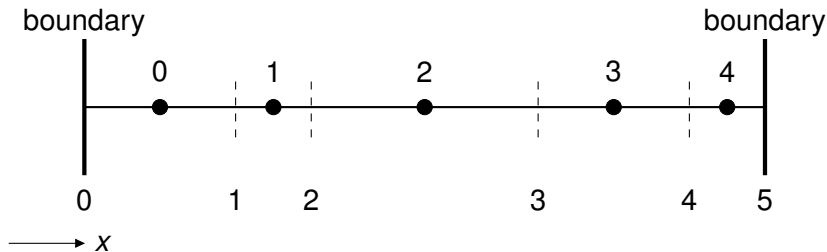


FIGURE: 1D grid.  $n_i=5$ . The bullets denote cell centers (and control volume) which are labeled 0–4. Dashed lines denote control volume faces labeled 0–5.

- The variables are stored in cells 0 – 4, e.g.  $u[0] - u[4]$ .
- No dummy nodes, i.e. no  $u[-1]$  and  $u[5]$ .
- Boundary conditions are introduced as source terms

GRID: WEST, EAST, SOUTH, NORTH ( $x - y$ )

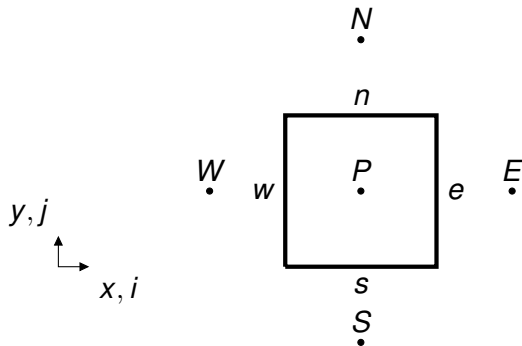
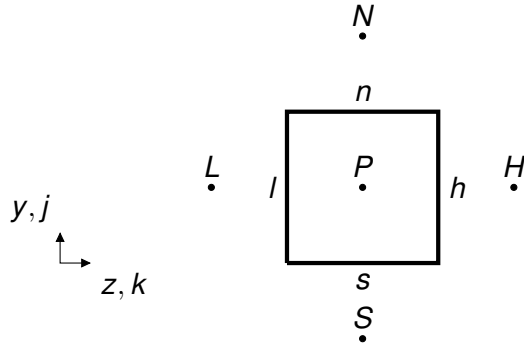


FIGURE: Control volume. Top:  $x - y$  plane; bottom:  $y - z$  plane.

## ► Interpolation

$$\phi_W = f_x \phi_P + (1 - f_x) \phi_W, \quad f_x = \frac{|\overrightarrow{WW}|}{|\overrightarrow{PW}| + |\overrightarrow{WW}|}$$

GRID: SOUTH, NORTH, LOW, HIGH ( $y - z$ )



# AREAS, VOLUME

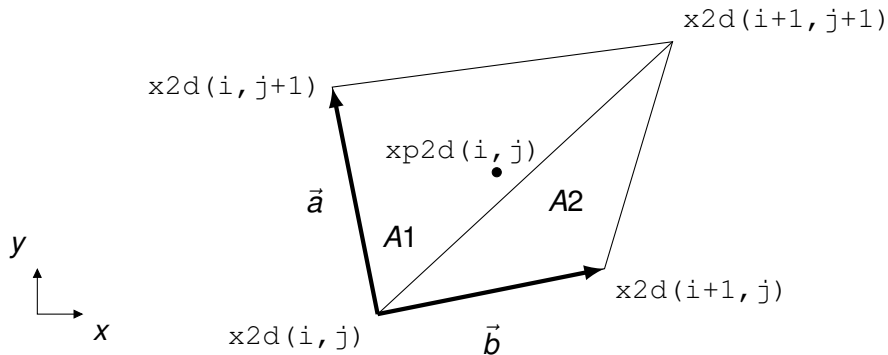


FIGURE: Calculation of areas and volume of cell  $i, j, k$ .

- The derivatives of  $\phi$  ( $\partial\phi/\partial x_i$ ) in a cell:

$$\frac{\partial\phi}{\partial x} = \frac{1}{V} \int_A \phi n_x dA, \quad \frac{\partial\phi}{\partial y} = \frac{1}{V} \int_A \phi n_y dA, \quad \frac{\partial\phi}{\partial z} = \frac{1}{V} \int_A \phi n_z dA$$

- For the x component, for example, we get

$$\frac{\partial\phi}{\partial x} = \frac{1}{V} (\phi_e A_{ex} - \phi_w A_{wx} + \phi_n A_{nx} - \phi_s A_{sx} + \phi_h A_{hx} - \phi_l A_{lx})$$

- The derivative  $\partial\phi/\partial x$ ,  $\partial\phi/\partial y$  and  $\partial\phi/\partial z$ , are computed in the Python modules `dphidx`, `dphidy` and `dphidz`, respectively.



# DISCRETIZED EQUATIONS

► They all read  $(u, v, w, k, \varepsilon, \omega)$

$$a_P \phi_P = a_E \phi_E + a_W \phi_W + a_N \phi_N + a_S \phi_S + a_H \phi_H + a_L \phi_L + S_U$$

$$a_P = a_E + a_W + a_N + a_S + a_H + a_L - S_P$$

- **Arrays:** `aw3d`, `ae3d`, ..., `ah3d`, `su3d`, `sp3d`
- $S = S_P \phi + S_U$
- Three different discretization schemes: central differencing scheme (CDS), 1st-order upwind, hybrid 1st-order upwind/CDS
- This is done in `coeff()`

## FLOW CHART FOR $\bar{u}$ IN MAIN

- compute convection  $\mathbf{u} \cdot \mathbf{A}$

```
convw, convs, convl=conv(u3d,v3d,w3d,p3d_face_w, ...
```

- boundary conditions

```
su3d, sp3d=bc(su3d, sp3d, u_bc_west, u_bc_east, u_bc_south ...
```

- Compute coefficients  $a_W, \dots a_H$

```
aw3d, ae3d, as3d, an3d, al3d, ah3d, apo3d, su3d, sp3d=coeff(convw, convs ...
```

- Add generic source, i.e.  $\partial \bar{p} / \partial x$

```
su3d, sp3d=calcu(su3d, sp3d, dpdx_old, p3d_face_w, p3d_face_s))
```

## FLOW CHART FOR $\bar{u}$ IN MAIN CONT'D

- Add Crank-Nicolson

```
ap3d,su3d=crank_nicol(u3d_old,aw3d,ae3d,as3d,an3d,al3d, ...
```

- Solve  $\bar{u}$

```
if solver_vel == 'pyamg':  
    u3d,residual_u=solve_pyamg(u3d,aw3d,ae3d,as3d,an3d,al3d,ah3d, ...  
elif solver_vel == 'pyamgx':  
    u3d,residual_u=solve_pyamgx(u3d,aw3d,ae3d,as3d,an3d,al3d, ...  
else:  
    # cgs, cg, gmres, qmr, lgmres  
    u3d,residual_u=solve_3d(u3d,aw3d,ae3d,as3d, ...)
```

## FLOW CHART FOR $\bar{p}$ /CONTINUITY EQ. IN MAIN

- Compute convection with new  $\bar{u}$ ,  $\bar{v}$ ,  $\bar{w}$

```
convw, convs, convl=conv(u3d,v3d,w3d,p3d_face_w,p3d_face_s,p3d_face_l)
```

```
if not cyclic_x:
```

```
    convw,u_bc_east = modify_outlet(convw)
```

- Compute convection with new  $\bar{u}$ ,  $\bar{v}$ ,  $\bar{w}$
- Compute continuity error

```
su3d=(convw[0:-1,:,:]-convw[1:,:,:]\ +convs[:,0:-1,:]-convs[:,1:,:]\  
      +convl[:, :, 0:-1]-convl[:, :, 1:]) /acrank/dt[itstep]
```

- $a_W, \dots a_H$  in Poisson  $\bar{p}$  eq.

```
if iter == 0 and itstep == 0:
```

```
    aw3d, ae3d, as3d, an3d, al3d, ah3d, su3d, ap3d=calcp(convw, convs, convl)
```

```
    aw3d_p=aw3d
```

```
    as3d_p=as3d
```

```
    al3d_p=al3d
```

## FLOW CHART FOR $\bar{p}$ /CONTINUITY EQ. IN MAIN CONT'D

- Solve Poisson  $\bar{p}$  eq.

```
if solver_p == 'pyamg':  
    p3d=solve_p(p3d,aw3d,ae3d,as3d,an3d,al3d, ...  
elif solver_p == 'pyamgx':  
    # the A matrix is re-computed in solve_pyamgx every time  
    aw3d,ae3d,as3d,an3d,al3d, ...  
elif solver_p == 'pyamgx_p':  
    # the A matrix computed only once (requires more GPUY memory)  
    p3d=solve_px(p3d,aw3d,ae3d,as3d,an3d,al3d,...
```

- Correct convections

```
convw,convs,convl,p3d,u3d,v3d,w3d,su3d= correct_conv(u3d,v3d,w3d ...
```

## FLOW CHART FOR $k - \omega$ MODEL. IN MAIN

- Compute turbulent viscosity

```
vis3d=vist_kom(vis3d,k3d,om3d)
```

- b.c. for  $k$

```
su3d,sp3d=bc(su3d,sp3d,k_bc_west,k_bc_east,k_bc_south,k_bc_north ...
```

- Compute  $a_W \dots a_H$  for  $k$

```
aw3d,ae3d,as3d,an3d,al3d,ah3d,apo3d,su3d,sp3d=coeff(convw,convsv,...
```

- Add generic sources, i.e.  $P^k$  and dissipation  $-C_\mu k\omega$

```
su3d,sp3d,gen,comm_term=calck_kom(su3d,sp3d,k3d,om3d,vis3d ...
```

## FLOW CHART FOR $k - \omega$ MODEL. IN MAIN CONT'D

- Add Crank-Nicolson

```
ap3d,su3d=crank_nicol(k3d_old,aw3d,ae3d,as3d,an3d,al3d, ...
```

- Solve  $k$  eq.

```
if solver_turb == 'pyamg':  
    k3d,residual_k=solve_pyamg(k3d,aw3d,ae3d,as3d,an3d,al3d,  
    ...
```

- The flow chart for  $\omega$  eq. is the same as for  $k$

## CALCU

```
def calcu(su3d, sp3d, dpdx_old, p3d_face_w, p3d_face_s):  
    # pressure gradient  
    dpdx=acrank*dphidx(p3d_face_w, p3d_face_s) + (1-acrank)*dpdx_old  
    su3d=su3d-dpdx*vol  
  
    # modify su & sp  
    su3d, sp3d=modify_u(su3d, sp3d)  
    # unsteady term added in crank_nicol  
  
    return su3d, sp3d
```



CALCK

```
def calck_kom(su3d, sp3d, k3d, om3d, vis3d, u3d_face_w, u3d_face_s, ...
# production term
dudx=dphidx(u3d_face_w, u3d_face_s)
dwdx=dphidx(w3d_face_w, w3d_face_s)
...

gen= (2.*(dudx**2+dvdy**2+dwdz**2)+(dudz+dwdx)**2+(dvdz+dwdy)**2+...
vist=xp.maximum(vis3d-viscos, 1e-10)
su3d=su3d+vist*gen*vol
# dissipation term
if sst or kom_des:
    sp3d=sp3d-fk3d*cmu*om3d*vol
else:
    sp3d=sp3d-cmu*om3d*vol
# modify su & sp
su3d, sp3d, comm_term=modify_k(su3d, sp3d, gen)
```

# PANS

- The destruction term in the  $\varepsilon$  eq. is modified:  $C_{\varepsilon 2} \Rightarrow C_{\varepsilon 2}^*$ . In `calceps` it reads

```
if pans:
    c2u=c_eps_1+fk3d*(fdampf2*c_eps_2-c_eps_1)
else:
    c2u=fdampf2*c_eps_2
```

- Turb. Prandtl numbers:  $(\sigma_k, \sigma_\varepsilon) \Rightarrow (\sigma_k f_k^2, \sigma_\varepsilon f_k^2)$  In `coeff` it reads ( $f_{k,limit}$  is, say, 0.2)

```
if prand_1 > 0:
    vis_turb=(vis3d-viscos)/prand
else:
    fk3d_local=xp.maximum(fk3d,fkmin_limit) #this limit is used only
    vis_turb=(vis3d-viscos)/xp.abs(prand)/fk3d_local**2
```

- This array is used both PANS and DES/IDDES .... It is computed in `compute_fk`

```
def compute_fk(k3d,eps3d,fk3d):
    if pans:
        L_t=k3d**1.5/eps3d
        psi=xp.maximum(1,L_t/(cdes*delta_max))
        fk3d=xp.maximum(1-(psi-1)/(c_eps_2-c_eps_1),0)
    if keps_des:
        r1=k3d**1.5/eps3d
        fk3d=xp.maximum(1,r1/(0.67*delta_max))
    if j10 < 0:
        j1=xp.abs(j10)
        fk3d[:,0:j1,:]=1
    fk3d=modify_fk(fk3d)
```

- IDDES is implemented in module `modify_fk` in  
`hump-IDDES-ni-583-go4hybrid-mesh-STG-dt-0.002-GPU/modify_case.py`

# INLET B.C.

**pyCALC-LES** flowchart [▶ Link](#)

- Section 3.6
- `module modify_inlet`

## pyCALC-LES flowchart [▶ Link](#)

- Section 3.7
- module `bc`
- It is set when `u_bc_west_type`, `u_bc_east_type` ... `om_bc_high_type` are set to 'd'

# OUTLET B.C.

**pyCALC-LES** flowchart [▶ Link](#)

- Section 5.2
- **module** `modify_outlet`

# THE SMAGORINSKY TURBULENCE MODEL

**pyCALC-LES** flowchart [▶ Link](#)

- Section 6
- module `vist_smag`

**pyCALC-LES** flowchart [▶ Link](#)

- Section 7
- module `vist_wale`



# $k - \varepsilon$ TURBULENCE MODEL

## pyCALC-LES flowchart [▶ Link](#)

- Section 8
- module `calck`
- module `calceps`
- module `vist_pans`
- module `modify_eps` (in directory `channel-950-k-eps-RANS*`)

# $k - \omega$ TURBULENCE MODEL

## pyCALC-LES flowchart [▶ Link](#)

- Section 10
- `module calck_kom`
- `module calcom`
- `module vist_kom`
- `module modify_om   su3d[:,0,:]=ap_max*6*viscos*k3d[:,0,:]  
/ (c_omega_2*dist3d[:,0,:]**2)`

# WALL FUNCTIONS

► See Section 11.14.1 in [1]

$y^+$ : wall-adjacent cell center at  $30 \leq y^+ \leq 200$

$\bar{u}$ : set the wall shear stress as  $\tau_w = \rho u_\tau^2$  (recall that  $\rho = 1$ ). The log-law reads

$$\frac{\bar{u}_P}{u_\tau} = \frac{1}{\kappa} \ln \left( \frac{E u_\tau y_P}{\nu} \right)$$

where  $E = 9$  and  $\kappa = 0.41$ .

- Can't express  $u_\tau$  explicitly; we must iterate

$$u_\tau = \frac{\kappa \bar{u}_P}{\ln \left( \frac{E u_{\tau, \text{old}} y_P}{\nu} \right)}$$

$k$ : set  $k$  at the wall-adjacent cells as  $k_P = C_\mu^{-1/2} u_\tau^2$

$\varepsilon$ : set  $\varepsilon$  at the wall-adjacent cells as  $\varepsilon_P = u_\tau^3 / (\kappa y_P)$

$\omega$ : set  $\omega$  at the wall-adjacent cells as  $\omega_P = C_\mu^{-1/2} u_\tau / (\kappa y_P)$ , see Eg. 3.27 in [2]

# SYNTHETIC INLET FLUCTUATIONS

**pyCALC-LES** flowchart [▶ Link](#)

- Section 11
- **module** `synt_fluct` **in file** `synt_fluct.py`

# REFERENCES

- [1] L. Davidson. **Fluid mechanics, turbulent flow and turbulence modeling**. eBook, Division of Fluid Dynamics, Dept. of Mechanics and Maritime Sciences, Chalmers University of Technology, Gothenburg, 2021.
- [2] L. Davidson. **An Introduction to Turbulence Models**. Technical Report 97/2, Dept. of Thermo and Fluid Dynamics, Chalmers University of Technology, Gothenburg, 1997.